



content (Acetic acid and EDTA). Therefore, it might be corrosive to the injection system. We used standard SY/T 5405-1996 [30], related to petroleum products corrosion test in Chinese oil fields to estimate its corrosion rates and speed at different temperatures using N80 steel. Temperatures were set using a static water bath.

The corrosion rate (C) and corrosion speed (vi) are given by:

Where, m_0 is the initial steel mass, m_1 masses difference, A_i the steel surface area and t the time difference. Figure 1 below, shows the used steel to test the corrosivity.

Corrosion inhibitors screening: To reduce the proven corrosivity of the removal solution, we used standard SY/T 5756-1995, related to corrosion inhibitors testing for Chinese oil fields, to screen two corrosion inhibitors used in the oil field and an ammonium salt ($C_3N_2H_4$).

Spectrophotometry: Turbidity is the measure of relative clarity of a liquid. It is an optical characteristic of water and is a measurement of the amount of light that is scattered by material in the water when a light is shined through the water sample. The higher the intensity of scattered light, the higher the turbidity [31].

To calculate the turbidity, formation and injected waters based on the ions compositions (Table 4) sheets received from the oil field [32], were synthesized. A digital turbidity meter SGZ-2 to was used and temperatures were set in a static water bath.

Schematic diagram: The main objective of the solution is to decrease the injection pressure on the oil field during water flooding by removing the plugging within the formation; we decided to simulate the reservoir and plugging conditions in the lab by running a sand pack flooding experiment [33,34]. The experiment was ran using the oil field sand at 60°C, which is the reservoir temperature. Figure 2 below, represents the scheme of the core.

The experiment was ran in four steps:

- Determine the initial sand permeability: The formation water was injected at 1 mL/min until the pressure got stable for at least 1 PV injection volume.

- Create an artificial plugging to increase the pressure, which will represent the plugging pressure: Mix the injected and formation waters at 50/50 ratio and inject the mixture at 1 mL/min to create an inorganic scale within the pack so to reach the highest pressure of the system.

- Test the injectivity of the solution at the plugging pressure: Inject the solution at 2mL/min for 3 PV and record the pressures.

- Restore the sand permeability: Inject the formation water at 1 mL/min until stability of the pressure system.

SEM & XRD: After filtration, the plug was found to be 38.74 Wt.% organic and 61.26 Wt.% inorganic: Images of the plugging of Images of the plugging material are shown in Figure 3 below.

SEM & XRD: Results of SEM & XRD analysis are below in Figures 4 and 5.

From SEM images, the structure of the scale is a dispersed group of spherical balls around a middle one bigger and more compact. Which makes it easy to be disengaged and hence dissolvable in weak acids.

After ZAF correction, the diagram tells that, the scale is oxygen 45.12 At%, carbon 22.54 At%, aluminum 15.99 At%, Silica 15.52 At% and iron 00.83 At%. That makes it an aluminum silicate scale of formula $SiO_x AlO_y$

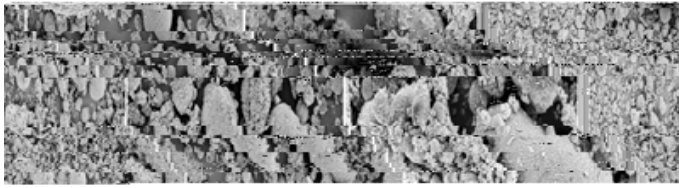


Figure 4: XRD diagram of the scale elements.

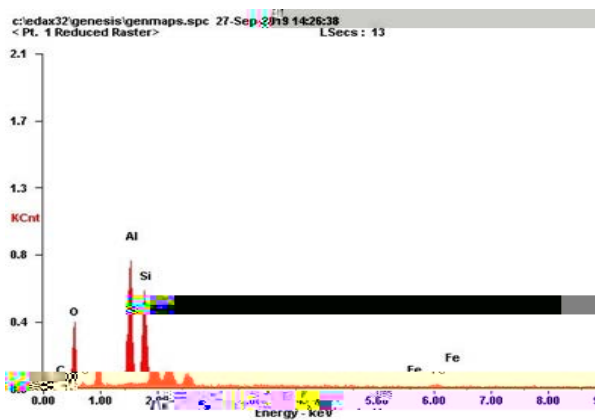


Figure 5: XRD diagram of the scale elements.

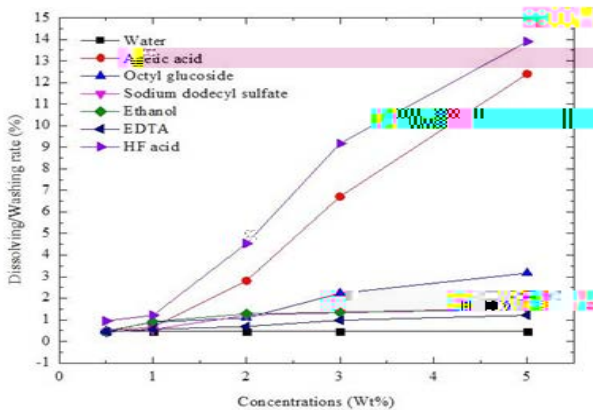


Figure 6: Chemicals dissolving/washing rates.

At low concentrations, acetic acid has shown the highest dissolve rate to the plug compared to the reference of HF acid. Then the glucoside surfactant and EDTA are the second and third respectively.

Figure 7: Dissolving/Washing rates of the five formulas are given in Figure 7 below.

From the diagram, the best combination to dissolve the scale was the Surfactant-Based Solution (SBS) with 63% of scale dissolved; it contains 5% Octyl glucoside, 2% acetic acid, 3% ethanol, 2% EDTA, and 3% sodium dodecyl sulfate.

Figure 8: The pH values with temperature change are given in Figure 8 below.

At room temperature, the solution had 6.34 pH, almost basic solution. Then with temperature increasing the pH decreased to 5.86 from 60°C to 70°C. That makes it indeed an acid solution at reservoir temperatures but still in the range of the oil field requirements [5].

Figure 9: Dissolution rates with temperature changes are in Figure 9 below.

As expected, change in temperatures affects the dissolving process as it increases gradually to reach 72% of scale dissolved at 120°C, while

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injection wells on platform B of Bohai oil field is due mostly to injected water suspended solids content, reservoir sensitivity to pro le control agents, incompatibility between injected and formation waters and acidizing operations. From this present work, we retained:

- The studied plugging sample is an inorganic scale of Aluminum silicate family.
- The new removal solution has good compatibility with formation and injected waters (9.8 NTU), good acid pH (5.8), low corrosion rate (2.12%) and dissolves until 72% of the scale plug.
- The solution has perfect injectivity to the formation sand and decreases the injection pressures of the system of 0.426 MPa within 3 PV of injected volume. It helps as well to restore permeability bigger to the initial permeability of the sand.
- From its characteristics and performances; the solution is good enough for immediate use on site for unplugging the formation during water flooding.

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A project submitted to our laboratory, the key laboratory of unconventional oil and gas development (China University of Petroleum (East China)), Qingdao 266580, PR China.

Conflicts of Interest

The authors declare that they have no conflict of interest.

References

1. Lu Q, Ning Y, Wang J, Yang X (2015) Scale removal technology for water injection wells in Bohai oilfield. *Oil Gas Res* 3: 312-323.
2. T Yi, Jin Z, Chuan-Li X, Wei-Ying W (2014) Scale removal technology for water injection wells in Bohai oilfield. *Pet Sci Technol* 32: 2512-2519.
3. Bin Merdhan AB, Mohd Yassin AA (2007) Scale formation in oil reservoir during water injection at high-salinity formation water. *J Appl Sci* 7: 3198-3207.
4. Li B, Kang X, Zhang J, Tang E, Wei Z, et al. (2018) A systematic study of the scale removal technology for water injection wells in Bohai oilfield. *Proc. - SPE Symp. Improv. Oil Recover.*
5. Yuan JB, Wood DA (2018) Overview of Formation Damage During Improved and Enhanced Oil Recovery. Elsevier Inc.
6. Dragomir A, Precupanu V, Arsenoiu V, Tippel P, Radulescu G, et al. (2013) Scale removal technology for water injection wells in burcioaia reservoir (romania) and research on damage removal methods. *SPE - Eur. Form. Damage Conf. Proceedings, EFDC* 1:126-146.
7. Nasr-El-Din HA, Al-Mohammad AM, Al-Hajri MA, Chesson JB (2005) A new chemical treatment to remove multiple damage in a water supply well. *SPE - Eur. Form. Damage Conf. Proceedings, EFDC*: 509- 517.
8. Mitchell RW, Grist DM, Boyle MJ (1980) Chemical Treatments Associated With North Sea Projects. *J. Pet. Technol* 32:904-912.
9. Yuan B, Wood DA (2018) A comprehensive review of formation damage during enhanced oil recovery. *J Pet Sci Eng* 167: 287-299.
10. Bedaiwi E, Al-Anazi B, Paiaman A, Al-Anazi A (2009) Polymer Injection for Water Production Control through Permeability Alteration in Fractured Reservoir. *Nafta* 60 pp: 221-231.

11. Chen T, Wang Q, Chang F, Al-Janabi Y (2016) Scale removal technology at High-Pressure, High Temperature. *Saudi Aramco Journal of Technology* pp: 47-54.
12. Aksland TG, Andrews JS (2006) Observations of well productivity and skin in wellbore area: A case study. *SPE Eighth Int. Symp. Oilf. Scale* 2006: 111-129.
13. Nasr-El-Din HA (2005) Formation damage induced by chemical treatments: Case histories. *J Energy Resour Technol Trans. ASME* 127: 214-224.
14. Yuan YS, Cao GS, Chen P, Gao Y (2014) A kind of novel chemical plugging solution for water injection wells. *Adv. Mater. Res* 884-885: 7-11.
15. Stalker R, Collins IR, Graham GM (2003) The Impact of Chemical Flooding on Well Productivity. *SPE Int. Symp. Oilf. Chem PP*: 441-453.
16. Yuan B, Wood DA (2018) A comprehensive review of formation damage during enhanced oil recovery. *J Pet Sci Eng* 167:287-299.
17. Moghadasi J, Muller-Steinhagen H, Jamaialahmadi M, Sharif A (2006) M, Sh00480